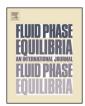
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# Partition study of textile dye Remazol Yellow Gold RNL in aqueous two-phase systems



Juliana Maria de Alvarenga <sup>a</sup>, Renata Aparecida Fideles <sup>a</sup>, Maira Vieira da Silva <sup>a</sup>, Gabriella Frade Murari <sup>a</sup>, Jason Guy Taylor <sup>a</sup>, Leandro Rodrigues de Lemos <sup>b</sup>, Guilherme Dias Rodrigues <sup>c</sup>, Aparecida Barbosa Mageste <sup>a,\*</sup>

- a Departamento de Química, ICEB, Universidade Federal de Ouro Preto, Campus Morro do Cruzeiro, CEP 35400-000 Ouro Preto, MG, Brazil
- <sup>b</sup> Departamento de Química, FACET, Universidade Federal dos Vales do Jequitinhonha e Mucuri Diamantina, MG, Brazil
- <sup>c</sup> Laboratório de Soluções Analíticas Verdes (LaSAV), Departamento de Química, Instituto de Ciências Exatas (ICEx), Universidade Federal de Minas Gerais (UFMG) Belo Horizonte, MG, Brazil

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#### ABSTRACT

The removal of organic dye pollutants from wastewater produced by the textile industry is a complex problem that presents potential health risks to the general public. Remazol Yellow Gold RNL (YR) dye is readily used to dye cellulose base materials and the methods developed for its removal from aqueous systems are either inefficient or too expensive to be adopted by smaller textile manufactures. Our approach is based on aqueous two-phase system (ATPS) using salts and either polymers or ionic liquids to extract Remazol Yellow Gold RNL from wastewater, Parameters such as the nature of the electrolyte, molecular mass of polymer and tie line length (TLL) on the dye partition coefficient  $(K_{YR})$  were all evaluated. A phase diagram for the polyethylene glycol (PEG 4000 g mol<sup>-1</sup>) and magnesiumsulfate system at 298.15 K was obtained and used to study the partitioning of YR. The  $K_{YR}$  values demonstrate the potential of both systems for the removal of dyes from industrial effluents. The partition mechanism was discussed based on the Haynes model and using the of Gibbs standard energy change ( $\Delta_{tr}G^{\circ}$ ). The driving force (enthalpy and/or entropy) that governs the partitioning of the dye depends on the nature of the ATPS. The optimized conditions that gave the best system was successfully applied to the removal of YR from wastewater obtained from a local textile manufacturer. The high  $K_{VR}$  values in the presence of the effluent demonstrate the potential and robustness of the ATPS for the treatment of effluents from textile industries.

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# 1. Introduction

Dyes are organic compounds that give color to materials and are used extensively in various industries such as textiles, cosmetics, paper and plastic industries [1]. Despite the wide application of dyes, their disposal into the environment and contamination of water is a major problem that has aroused concern due to their adverse effects on human health, to fauna and to flora [2,3]. In view of the toxicity and undesirable effects to aquatic environments, environmental regulations have become increasingly stricter [4] and spurred a demand for efficient methodologies for the removal of toxic waste products.

The removal of dyes from wastewater is a complex problem to resolve and different physicochemical processes such as [5]; adsorption [6], electrokinetic coagulation [7], ion exchange [8], electrochemical oxidation [9] and photocatalytic degradation [10] studies are routinely carried out to find solutions to this environmental problem [5]. However, these methodologies have their drawbacks, amongst which, the generation of hazardous waste or secondary intermediates, slow degradation rates and high costs are limitations that stand out. In this sense, new and more efficient methods that are cleaner, safer and economically viable are required for removing dyes from industrial effluents before releasing them into water bodies.

Aqueous two-phase system (ATPS) may be formed by mixing aqueous solutions of an electrolyte and a polymer. Alternatively, aqueous solutions of two chemically different polymers can be mixed to prepare ATPS or they may be formed from two kinds of

<sup>\*</sup> Corresponding author. Tel.: +55 31 3559 1707; fax: +55 31 3559 1707. E-mail address: aparecida@iceb.ufop.br (A.B. Mageste).

salts mixed under certain thermodynamic conditions, e.g. temperature, pressure and composition [11]. In recent years, new type of ATPS containing salts and ionic liquid (IL) (IL–ATPS) have been investigated [12]. The resulting system consists of two immiscible phases, with the major component of these systems being essentially water. ATPS are environmentally safe, recyclable, economical viable, quick and scalable for application in industrial processes [13].

Mageste et al. [14,15] evaluated the partition behavior of natural dye carmine and norbixin in different ATPS systems formed from polymer and salts. A significant transfer of dyes to the upper phase of the ATPS was observed and thus demonstrating the potential of these systems for purification applications. ATPS systems formed by potassium salts and polyethylene glycol (PEG) using ionic liquids as adjuvant have also been reported by Souza et al. [16] for the partitioning of dyes chloranilic acid and rhodamine 6G. Recently, Ferreira et al. [4] achieved extraction efficiencies of 100% when employing IL–ATPS for the extraction of dyes chloranilic acid, indigo blue and sudan III. In respect of these systems, little is known about the driving force that dictates how these dyes partition between the phases. Understanding these parameters is of fundamental importance to allow the full potential use of ATPS systems in large scale to be realized.

To the best of our knowledge, there are no reports in the literature concerning the use of ATPS for the removal of dye Remazol Yellow Gold (RNL or YR), also known as Remazol Golden Yellow (Fig. 1) from wastewaters. This dye is commonly used in the textile industry for dyeing cellulose fibers. The removal of Remazol Yellow Gold RNL from aqueous solutions has been accomplished by adsorption [17], anaerobic degradation [18] and photocatalytic approaches [19].

Thus, the aim of this study was to investigate the driving forces that determine the partition behavior of YR in ATPS composed of either polymer+salt or salt+ionic liquid. Herein, we report the effects of the nature of the electrolyte, average molar mass of the polymer and the system composition on the dye extraction yield. Furthermore, a phase diagram for the PEG 4000+magnesium sulfate salt+water at 298.15 K system was determined to study the effect of polymer molar mass. In order to demonstrate the robustness of ATPS, partition experiments were carried out using industrial (effluent) samples obtained from a local textile manufacturer in the city of Itabirito, Minas Gerais, Brazil.

#### 2. Material and methods

# 2.1. Materials

Polyethylene glycol (PEG) with an average molecular weight of 1500, 4000 and  $6000\,\mathrm{g\,mol^{-1}}$  were used. Ammonium sulfate ((NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>), lithium sulfate monohydrate (Li<sub>2</sub>SO<sub>4</sub>·H<sub>2</sub>O), magnesium sulfate heptahydrate (MgSO<sub>4</sub>·7H<sub>2</sub>O), sodium citrate (NaH<sub>2</sub>C<sub>6</sub>H<sub>5</sub>O<sub>7</sub>), sodium sulfate (Na<sub>2</sub>SO<sub>4</sub>) and sodium tartarate dihydrate (Na<sub>2</sub>C<sub>4</sub>H<sub>4</sub>O<sub>6</sub>·2H<sub>2</sub>O) were purchased from Synth (SP, Brazil). n-Bromobutane, methylimidazole, sodium tetrafluoroborate, dichloromethane were purchased from Sigma–Aldrich (St. Louis,

Fig. 1. Chemical structure of Remazol Yellow Gold RNL dye.

MO, USA). Wastewater and dye YR,  $C_{16}H_{18}N_4O_{10}S_3 \cdot Na_2$ , were kindly provided by a textile manufacturer located in Itabirito city, MG, Brazil. The YR chemical structure is shown in Fig. 1. Distilled water was used for every experiment. All chemicals used in this study were of analytical grade and used without further purification. Ionic liquid 1-butyl-3-methylimidazolium tetrafluoroborate ([Bmim] BF<sub>4</sub>) was synthesized in our laboratory and was purified according to the methods reported in the literature [20].

# 2.2. Synthesis and spectral characterization of ionic liquid 1-butyl-3-methylimidazolium tetrafluoroborate

The method described by Burrell et al. [20] was adopted with minor modifications. n-Bromobutane (30 g) was slowly added by addition funnel to freshly distilled methylimidazole (25 g) in a 250 mL two-necked round-bottom flask fitted with a reflux condenser. An ice water bath was used to prevent the temperature of the solution rising above 40 °C. This mixture was then stirred with a magnetic stirrer at room temperature for 30 h. The ionic liquid was then dissolved in deionized water (300 mL) and decolorizing charcoal (10 g) was added to the solution, which was heated at 60 °C for 2 h. The mixture was then cooled to room temperature and filtered. The colorless 1-butyl-3-methylimidazolium bromide solution was then poured into a solution of sodium tetrafluoroborate (34g) in 250 mL of deionized water and stirred at room temperature for 3 h. The solution was transferred to separatory funnel and extracted with dichloromethane  $(3 \times 70 \,\mathrm{mL})$ . The organics were combined and filtered through a plug of silica (100 g) to remove sodium bromide. The dichloromethane solution was dried in vacuo to give neat 1-butyl-3methylimidazolium tetrafluoroborate as a transparent viscous liquid (74% yield).  $\delta_{\rm H}$  (250 MHz, CDCl<sub>3</sub>): 8.85 (1H, s), 7.33–7.42 (2H, m), 4.19 (2H, t, J 7.5), 3.96 (3H, s), 1.79-1.92 (2H, m), 1.30-1.41 (2H, m), 0.96 (3H, t, J 7.3);  $\delta_C$  (62.5 MHz, CDCl<sub>3</sub>): 136.6, 123.5, 121.9, 49.9, 36.3, 31.9, 19.4, 13.3. Nuclear magnetic resonance (NMR) spectra were measured at 250 MHz (1H), on a Bruker 250 spectrometer, All NMR spectra were recorded in CDCl<sub>3</sub>, with reference to tetramethylsilane. NMR data are in accordance with literature values [20]. The purity (>98%) of the ionic liquid was determined by integration of <sup>1</sup>H NMR signals.

# 2.3. Determination of ATPS phase diagrams

The systems used to evaluate partitioning behavior of the dye have been summarised in Table 1. Most of the phase diagrams pertinent to this study have been previously reported in the literature [21–27]. Phase diagrams for the PEG 4000+magnesium sulfate+water system at 298.15 K were obtained and utilized in

**Table 1**Summary of the ATPS utilized for the partitioning of YR.

```
PEG 1500 + Li<sub>2</sub>SO<sub>4</sub> + water* [23]
PEG 1500 + NaH<sub>2</sub>C<sub>6</sub>H<sub>5</sub>O<sub>7</sub> + water* [25]
PEG 1500 + Na<sub>2</sub>C<sub>4</sub>H<sub>4</sub>O<sub>6</sub>·2H<sub>2</sub>O + water* [25]
PEG 1500 + Na<sub>2</sub>SO<sub>4</sub> + water* [23]
PEG 1500 + (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub> + water* [27]
PEG 1500 + (MgSO<sub>4</sub> + water* [23]
PEG 4000 + MgSO<sub>4</sub> + water* [23]
PEG 4000 + MgSO<sub>4</sub> + water* [24]
PEG 6000 + H<sub>2</sub>SO<sub>4</sub> + water* [24]
PEG 6000 + Li<sub>2</sub>SO<sub>4</sub> + water* [22]
PEG 6000 + Li<sub>2</sub>SO<sub>4</sub> + water* [24]
([Bmim]BF<sub>4</sub> + (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub> + water* [26]
([Bmim]BF<sub>4</sub> + MnSO<sub>4</sub> + water* [21]
```

<sup>\*</sup>Phase diagrams were obtained from the literature [references].

YR partitioning studies. Stock solutions of the polymer and salt were prepared by weighing known quantities of the reagents on an analytical balance (Shimadzu, AG 220 with an uncertainty of  $\pm 0.0001\,\mathrm{g}$ ). This stock solution and water were then mixed in glass tubes. The tubes were vigorously shaken and kept in a thermostatic bath (Marconi, MA 184, with an uncertainty of  $\pm 0.1\,\mathrm{K}$ ) at 298.15 K for at least 48 h to guarantee complete separation of the phases and the realization of a thermodynamic equilibrium. Next, the two phases were separately collected for analysis.

The composition of the each separated phases was quantified in two steps: (i) the phases were separately collected and diluted to determine the salt concentration by conductivity analysis performed at 298.15 K (Schott CG853, Germany). (ii) The water content was determined by volatilization gravimetry in an oven at 343.15 K until constant weight was achieved. The polymer concentration  $(W_{\text{PEG}})$  in the phases was determined by mass difference for each component,  $w_{\text{PEG}} = w_{\text{total}} - w_{\text{H}_2\text{O}} - w_{\text{salt}}$  where  $w_{\text{total}} = 1.00$ .

The tie line length (TLL) was calculated according to Eq. (1).

$$TLL = \left[ \left( C_{P}^{T} - C_{P}^{B} \right)^{2} + \left( C_{S}^{T} - C_{S}^{B} \right)^{2} \right]^{1/2}$$
 (1)

where  $C_P^T$  and  $C_P^B$  are the concentrations of polymer and  $C_S^T$  and  $C_S^B$  are the salt concentration in the top and bottom phases, respectively.

#### 2.4. Partition experiments

#### 2.4.1. Preparation of stock solutions

All PEG and salt concentrations in stock solutions are represented in weight percent. Appropriated amounts of PEG and salt were dissolved in distilled water to prepare the stock solutions. The dye solution was obtained by dissolving  $0.4\,\mathrm{g}$  of YR in approximately  $2.25\,\mathrm{g}$  of water. The resultant concentration was  $3.13\,\mathrm{mmol\,kg^{-1}}$ .

# 2.4.2. Preparation of aqueous two-phase systems (ATPS)

To achieve the desired compositional ratio for each ATPS [21–26], appropriate amounts of [Bmim]BF<sub>4</sub> or PEG, salt stock solutions and water were taken into a graduated centrifuge tubes. The tubes were shaken and left to stand in a thermostatic bath at 298.15 K, for a minimum of 48 h (Marconi, MA 184, with an uncertainty of  $\pm 0.1$  K). Once the system had achieved thermodynamic equilibrium, the two phases were collected separately for partitioning experiments.

# 2.4.3. Partition behavior of Remazol Yellow Gold RNL in ATPS

For partition studies of ATPS containing polymer+salt+water, the samples were prepared by mixing 3.0 g of both top and bottom phases of ATPS and adding 100 mg of dye solution. In the case of ATPS formed by IL, 0.033 g of YR solution was added to the system that contained 1.0 g of each phase. For each TLL and each ATPS, three systems were prepared: the first being a blank without the addition of the dye, a sample and a replica. The mixtures were stirred manually for 3 min until the solutions became cloudy and then maintained under controlled temperature in a thermostatic bath at 298.15 K. After a period of 48 h, phase separation occurred and the thermodynamic equilibrium was reached. Both phases were collected separately and diluted in order to determine the dye concentration. The dye was quantified in each phase using a UV-vis spectrophotometer (Hewlett Packard 8453) at a wavelength of 256 nm.

The partition coefficient for the dye ( $K_{YR}$ ) between the phases is determined by the concentration ratio of the analyte in each phase of the ATPS as described in Eq. (2).

$$K_{\rm YR} = \frac{\left[{\rm YR}\right]^{\rm T}}{\left[{\rm YR}\right]^{\rm B}} \tag{2}$$

where  $[YR]^T$  and  $[YR]^B$  express the dye concentration in the upper and lower phases respectively. In agreement with the Beer– Lambert law, the absorbance of the analyte at a specific wavelength is directly proportional to the analyte concentration. Thus, the partition coefficient  $(K_{YR})$  can be given as described in Eq. (3).

$$K_{\rm YR} = \frac{{\rm Abs_T} f_{\rm dTP}}{{\rm Abs_R} f_{\rm dBP}} \tag{3}$$

where  ${\rm Abs_T}$  and  ${\rm Abs_B}$  are the absorbance of the upper and lower phases respectively at the specified wavelength. Terms  $f_{\rm dTP}$  and  $f_{\rm dBP}$  express the dilution factors for each phase.

# 2.5. Recovery experiments

#### 2.5.1. Preparation of waste water solution and stock solutions

The waste water was filtered and then diluted ten times. This waste water stock solution was then kept under refrigeration. Dye, PEG 1500 and lithium sulfate stock solutions were prepared using waste water stock solution as solvent in the same manner as described previously.

# 2.5.2. Recovery of YR in presence of waste water

To investigate the recovery of YR, a PEG  $1500 + \text{Li}_2\text{SO}_4 + \text{H}_2\text{O}$  ATPS mixture doped with YR was used. The partition procedure was performed as previously described. After separation of the two-phases, the dye was quantified in each phase using a UV–vis spectrophotometer at a wavelength set at 256 nm. The concentration of dye YR in each phase was determined from a linear calibration curve.

The recovery percentage (%R) of the YR was calculated by Eq. (4).

$$\%R = \frac{n_{\rm T}}{n_{\rm Tot}} \times 100 \tag{4}$$

where  $n_{\rm T}$  is the amount of dye present in the top phase and  $n_{\rm Tot}$  is the total amount of dye added to the system.

# 2.6. Extraction efficiency of YR in ATPS

The extraction efficiency for YR in each ATPS is expressed by the relation between the amount of dye present in the upper phase to the total quantity of dye in the ATPS at thermodynamic equilibrium. This parameter is obtained as described by Eq. (5) [4].

$$\%E_{YR} = \frac{Abs_T f_{dTP} \times w_T}{(Abs_T f_{dTP} \times w_T) + (Abs_B f_{dTB} \times w_B)} \times 100$$
 (5)

where  $\mathrm{Abs}_{\mathrm{T}}f_{\mathrm{dTP}}$  and  $\mathrm{Abs}_{\mathrm{B}}f_{\mathrm{dTB}}$  are the absorbance's of the superior and inferior phases and  $w_{\mathrm{T}}$  and  $w_{\mathrm{B}}$  represent the mass of the upper and lower phases, respectively.

#### 2.7. YR transfer Gibbs standard energy change ( $\Delta_{tr}G^{\circ}$ )

For all ATPS studied, the Gibbs standard energy change ( $\Delta_{tr}G^{\circ}$ ) was obtained following the thermodynamic relationship:

$$\Delta_{\rm tr}G^{\circ} = -RT\ln K_{\rm YR} \tag{6}$$

where R is the universal gas constant, T is the absolute temperature and  $K_{YR}$  is the dye partition coefficient.

The thermodynamic parameter  $\Delta_{tr}G^{\circ}$  is the change in the Gibbs energy of the system when 1 mol of dye, under infinite dilution is transferred from the bottom phase to the top.

**Table 2** Equilibrium data for PEG  $4000(w_{PEG})$  + magnesium sulfate  $(w_s)$  + water  $(w_W)$  system to 298.15 K.

	Overall			Top phase			Bottom phase		
TLL	100 w <sub>PEG</sub>	100 w <sub>s</sub>	100 w <sub>w</sub>	100 w <sub>PEG</sub>	100 w <sub>s</sub>	100 w <sub>w</sub>	100 w <sub>PEG</sub>	100 w <sub>s</sub>	100 w <sub>w</sub>
43.85	22.05	8.91	69.04	41.44	0.81	57.75	1.81	19.57	78.62
48.12	24.59	9.48	65.93	45.00	0.53	54.47	1.26	20.58	78.16
50.53	25.82	9.82	64.36	46.59	0.44	52.97	1.23	22.71	76.06
53.31	26.69	10.80	62.51	49.87	0.31	49.83	1.96	23.69	74.36
55.28	28.60	11.53	59.87	51.33	0.19	48.48	2.29	25.70	72.00

Standard deviations of the salt and polymer concentration are lower than  $\pm 0.76$  and  $\pm 2.2$ , respectively.

#### 3. Results and discussion

# 3.1. Phase diagrams

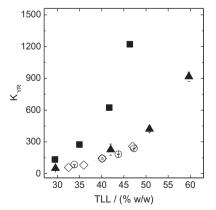
The phase compositions for the ATPS formed by PEG 4000 and magnesium sulfate salt are shown in Table 2. All concentrations are expressed in weight percent. This data is of fundamental importance for studying partition and extraction of solutes in ATPS. Water is the major component in both phases. The upper phase is enriched with polymer whereas the bottom phase is rich in salt. This behavior is in agreement with other observations made for polymer/salt ATPS systems [22–25].

# 3.2. The tie line length effect on the partitioning YR

The tie line length (TLL) is a line that connects the points of the diagram which represent the composition of the two phases at thermodynamic equilibrium. The TLL is an important thermodynamic parameter that indicates which distinct and intensive thermodynamic properties of the phases co-exist at equilibrium [14].

Fig. 2 shows the partition coefficient values for YR at 298 K as a function of the tie line length in ATPS formed by PEG 1500 + sulfate salts +  $\rm H_2O$ . When analyzing the partition behavior of YR, it can be seen that a rise in tie line length significantly increases the dye transference to the top phase of the ATPS. Furthermore, it is important to note that the YR preferentially partitions to the top phase. All of the systems formed by polymer+salt showed  $K_{\rm YR}$  values greater than unity, indicating the affinity of the dye for the top phase of the system and the potential of ATPS for the extraction of this dye.

For a better understanding of the partition mechanism of YR in this ATPS, the thermodynamic parameter  $\Delta_{tr}G^{\circ}$  was determined. The Gibbs standard energy change of transfer ( $\Delta_{tr}G^{\circ}$ ) at 298.15 K as



**Fig. 2.** Effect of cation of the salt forming ATPS on the YR partition behavior: (■) PEG  $1500 + \text{Li}_2\text{SO}_4 + \text{H}_2\text{O}$ , (○) PEG  $1500 + \text{Mg}\text{SO}_4 + \text{H}_2\text{O}$ , (▲) PEG  $1500 + (\text{NH}_4)_2\text{SO}_4 + \text{H}_2\text{O}$ , (◇) PEG  $1500 + \text{Na}_2\text{SO}_4 + \text{H}_2\text{O}$ .

a function of the TLL for all the ATPS studied are presented below (Table 3).

The negative values of  $\Delta_{tr}G^\circ$  indicate that the partitioning of YR in ATPS formed by PEG + salts + H\_2O is spontaneous. Partitioning of YR occurs when there is a decrease in the Gibbs energy of the system. We can understand why this dye prefers the top phase of the ATPS over the bottom phase by evaluating the factors that contribute to  $\Delta_{tr}G^\circ$ , i.e. the contribution of  $\Delta_{tr}H^\circ$  and  $\Delta_{tr}S^\circ$ . In general, results show a reduction in the  $\Delta_{tr}G$  value with increasing TLL, except for the case involving ATPS containing ionic liquids ([Bmim]BF\_4+MgSO\_4+H\_2O. For ATPS with polymer, salt and water, the  $\Delta_{tr}G^\circ$  values are negative and demonstrate the spontaneous transfer of the dye to the top phase of the system. As shown in Table 3, for ATPS formed from IL,  $\Delta_{tr}G^\circ$  are positive due to inversion in the tendency of YR to partition to top phase.

The driving forces that direct the partition of the solute in the ATPS can be evaluated qualitatively by a simple model developed by Johansson et al., which is derived from the Flory–Huggins theory [28]. This model relates the partition coefficient of the solute to enthalpic and entropic contributions.

The entropic contribution for solute partitioning is described by Eq. (7).

$$\ln K_{\rm YR} = \frac{M_{\rm YR}}{\rho} \left( \frac{n^{\rm T}}{V^{\rm T}} - \frac{n^{\rm B}}{V^{\rm B}} \right) \tag{7}$$

where  $M_{\rm YR}$  is the molecular weight of the solute partitioned,  $n^{\rm T}$  and  $n^{\rm B}$  are the total number of molecules in the top and bottom phases and are divided by the  $V^{\rm T}$  and  $V^{\rm B}$  density number of each phase. Finally,  $\rho$  is the number of lattice sites per unit volume.

This equation shows that in the absence of an enthalpic contribution, the heterogeneous distribution of a solute between the phases will occur if there is a density difference between the phases. In the more dense phase, there are a greater number of different configurations to distribute the molecules that constitute the ATPS and the solute [28]. In ATPS formed by PEG+salts+ $H_2O$ , the number density in the bottom phase is higher than the top phase due to the higher water content of the salt-rich phase

**Table 3** Variation of Gibbs standard free energy,  $\Delta_{\rm tr}G^{\circ}$ , (kJ mol $^{-1}$ ) of transfer YR for all systems at 298.15 K and different TLL values.

ATPS	TLL 1	TLL 2	TLL 3	TLL 4	TLL 5
PEG 1500 + Li <sub>2</sub> SO <sub>4</sub>	-12.12	-13.91	-15.95	-17.61	
PEG 1500 + NaH <sub>2</sub> C <sub>6</sub> H <sub>5</sub> O <sub>7</sub>	-8.901	-10.11	-11.87	-13.43	-14.89
PEG	-7.82	-10.14	-12.03	-12.93	-13.35
1500 + Na <sub>2</sub> C <sub>4</sub> H <sub>4</sub> O <sub>6</sub> ·2H <sub>2</sub> O					
PEG 1500 + Na <sub>2</sub> SO <sub>4</sub>	-10.08	-10.89	-12.32	-13.75	-14.33
PEG $1500 + (NH_4)_2SO_4$	-9.74	-13.44	-14.97	-16.89	
PEG 1500 + MgSO <sub>4</sub>	-11.03	-12.29	-12.91	-13.56	-14.33
PEG 4000 + MgSO <sub>4</sub>	-13.09	-13.36	-14.19	-14.83	-15.28
PEG 6000 + MgSO <sub>4</sub>	-9.88	-10.68	-11.48	-12.46	-13.16
PEG 4000 + Li <sub>2</sub> SO <sub>4</sub>	-13.91	-15.20	-16.63	-17.38	
PEG 6000 + Li <sub>2</sub> SO <sub>4</sub>	-14.16	-14.67	-15.97	-17.12	
IL + (NH4)2SO4	8.501	6.39	5.89		
IL+MnSO <sub>4</sub>	4.139	4.413	4.994	5.030	5.823

**Table 4** Difference in the concentration of  $H_2O$  between the bottom and top phases of the ATPS, at 298.15 K.

ATPS	TLL					
	1	2	3	4	5	
PEG 1500 + NaH <sub>2</sub> C <sub>6</sub> H <sub>5</sub> O <sub>7</sub>	10.9	13.95	15.02	16.08	16.93	
PEG 1500 + $Na_2C_4H_4O_6 \cdot 2H_2O$	13.4	15.19	16.95	18.25	18.54	
PEG 1500+(NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub>	12.95	17.05	17.35	20.51	20.98	
PEG 1500 + Na <sub>2</sub> SO <sub>4</sub>	17.1	16.78	18.58	22.13	23.32	
PEG 1500 + MgSO <sub>4</sub>	15.97	19.88	21.87	22.13	25.09	
PEG 1500 + Li <sub>2</sub> SO <sub>4</sub>	17.35	19.88	22.42	24.65	27.69	
PEG 4000 + Li <sub>2</sub> SO <sub>4</sub>	22.16	24.43	26.27	28.64	30.66	
PEG 6000 + Li <sub>2</sub> SO <sub>4</sub>	22.29	23.94	25.36	26.91	29.32	
PEG 4000 + MgSO <sub>4</sub>	20.87	23.69	23.09	24.53	23.53	
PEG 6000 + MgSO <sub>4</sub>	17.35	18.28	18.99	20.03	21.25	
IL + (NH4)2SO4	37.45	33.48	28.93			
IL+MnSO <sub>4</sub>	-39.92	-43.39	46.31	47.98	51.1	

(Table 4). In accordance with Eq. (7), there is a strong entropic contribution for solute partitioning to the bottom phase. However, the experimental results demonstrate that when the dye is introduced into this system, it moves to the top phase and thus decreases the entropy of the system.

Once the dye transfer process to the top phase becomes entropically unfavorable, enthalpy should be the driving force that governs dye partitioning to the polymer-rich phase. The enthalpic contribution is expressed in the Johansson et al. model [28], by

$$lnK_{YR} = -\frac{M_{YR}}{RT} \left[ \sum_{i=1(i \neq YR)}^{m} (\Phi_i^T - \Phi_i^B) W_{iYR} - \sum_{i=1(i \neq YR)}^{m} \sum_{j=i+1(j \neq YR)}^{m-1} (\Phi_i^T \Phi_j^T - \Phi_i^B \Phi_j^B) W_{ij} \right]$$
(8)

where  $\Phi_i^{\rm T}$  and  $\Phi_i^{\rm B}$  are the volume fraction of components that form the ATPS top and bottom phases, respectively,  $w_{ij}$  is the energy involved in the formation of effective pair potential which is defined as:  $w_{ij} = z[\varepsilon_{ij} - (1/2)(\varepsilon_{ii} + \varepsilon_{jj})]$ , z is the number of close neighbors, and  $\varepsilon_{ij}$  is the potential energy of the pair i-j.

The enthalpic driving force for solute partitioning is composed of two terms: (i) The first,  $\sum_{i=1(i \neq {\rm YR})}^m (\Phi_i^{\rm T} - \Phi_i^{\rm B}) W_{\rm iYR}$ , is the summation of the energy involved in the interaction between the YR solute and every component present in each phase of the ATPS. The second,  $\sum_{i=1(i\neq YR)}^{m}\sum_{j=i+1(j\neq YR)}^{m-1}(\Phi_i^T\Phi_j^T-\Phi_i^B\Phi_j^B)W_{ij}$ , represents the self-energy of the phase and an equivalent to the sum of the energy of the interaction between all the potential pairs formed by combination of the components in each phase in the absence of solute. The transfer of solute molecules from one phase to another changes the self-energy of the phase by breaking interactions between the components and concurrently forming new solute-component interactions. In other words, the partitioning of the dye requires breaking interactions between the original components to create a cavity into which the dye may fit. Eq. (8) predicts that the solute will favor partitioning to the phase where the component most strongly interacts and prefers the phase where there is less energy expenditure to form the cavity in which it is to be housed.

The fact that the dye displays higher affinity for the top phase ( $K_{YR}$  values greater than one) is explained by a specific interaction between polymer and YR molecules and the lower energy required to form a cavity that accommodates the dye in the top phase. As clearly observed in Fig. 2, an increase in the TLL leads to a significant increase in  $K_{YR}$  values. Given that TLL increases as a function of polymer and salt concentration, it seems reasonable to suggest that preferential migration to the top phase is due to interactions with polymer macromolecule and therefore giving rise to the formation of polymer–dye complexes in the top phase.

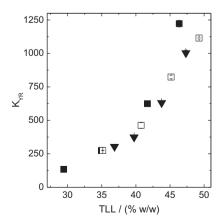
# 3.3. Effect of ATPS-forming electrolyte on the extraction of YR

Several researchers have studied the influence of the type of salts in ATPS on the extraction of solute [14,15,29]. PEG 1500 and sulfate salt were used for YR partition to investigate the effect of different cations on ATPS partitioning. The results are summarized in Fig. 2 and indicate that ATPS formed by lithium salt is more efficient in the transfer of YR to the top phase.

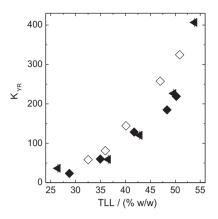
This cation effect may be explained by the model of da Silva and Loh [30], which suggests that when mixing the polymer and salt, the cation of the salt and the macromolecules interact to release water molecules that were previously solvating such components and therefore increase the entropy of the system. As the concentration of the electrolyte increases, the process continues until it reaches an energetic saturation. This is due to the effect of repulsive forces between polymer cation complexes and the added salts. Once the saturation point is reached, the addition of more electrolyte ions causes them to group together in a region furthest away from the macromolecule-ion complex. The addition of more electrolyte forms two phases and lowers the Gibbs energy of the system. When compared to other cations, the model indicates that a higher concentration of Li<sup>+</sup> is necessary to energetically saturate the polymer chain. Thus, the macromolecule structure of the polymer is more positively charged in the ATPS when composed of Li<sub>2</sub>SO<sub>4</sub> and this enables a stronger electrostatic interaction between the polymer-cation and YR in the Li<sub>2</sub>SO<sub>4</sub> system.

# 3.4. Molecular mass polymer effect

Fig. 3 shows the partition behavior of YR in the aqueous twophase systems formed by sulfate salts and polymer PEG with different molecular masses. If the polymer molecular weight is increased, the entropy of mixing solute and polymer will be reduced in the phase containing polymer. Moreover, there will be a reduction in the number of possible configurations for the dye molecules in the top phase, which thereby improves solute partition to the bottom phase [31]. Furthermore, the polymer becomes more hydrophobic with increasing molecular weight and increasing the hydrophobicity of the upper layer of ATPS. The YR is a highly hydrophilic species, so  $K_{YR}$  tends to decrease with increasing molar mass of the macromolecule. However, as can be observed in Fig. 3, there is no significant effect of the macromolecular size on the YR partitioning behavior. This partitioning behavior reinforces the idea that the YR transfer process to the top phase of the ATPS is enthalpy driven.



**Fig. 3.** Effect of PEG molar weight forming ATPS on the YR partition behavior: (■) PEG 1500 + Li<sub>2</sub>SO<sub>4</sub> + H<sub>2</sub>O, (□) PEG 4000 + Li<sub>2</sub>SO<sub>4</sub> + H<sub>2</sub>O, (▼) PEG 6000 + Li<sub>2</sub>SO<sub>4</sub> + H<sub>2</sub>O.



**Fig. 4.** Effect of anion of the salt forming ATPS on the YR partition behavior: ( $\diamond$ ) PEG 1500 + Na<sub>2</sub>SO<sub>4</sub> + H<sub>2</sub>O, ( $\blacktriangleleft$ ) PEG 1500 + NaH<sub>2</sub>C<sub>6</sub>H<sub>5</sub>O<sub>7</sub> + H<sub>2</sub>O, ( $\spadesuit$ ) PEG 1500 + Na<sub>2</sub>C<sub>4</sub>H<sub>4</sub>O<sub>6</sub>·2H<sub>2</sub>O + H<sub>2</sub>O.

# 3.5. Anion effect

Effect of anion on the partition of YR in ATPS formed by PEG 1500 and sodium salts are shown in Fig. 4.

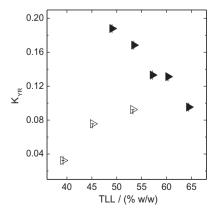
Results suggest that changing the anion of the salt does not significantly alter the partition behavior in the ATPS. This fact confirms the initial hypothesis that the partitioning of the dye occurs preferentially to the top phase due to a specific interaction between this solute and the polymer macromolecule.

# 3.6. Partition behavior of YR in IL–salt aqueous two-phase system (IL–ATPS)

After their application in 2003 [12], the IL–ATPS system has aroused much interest in the scientific community. They have been successfully employed to separate several solutes such as: sulfonamides in milk [32], cytochrome C [33], bovine serum albumin [34], antibiotics in honey [35], textile dyes [4], among others.

Fig. 5 shows the partition behavior of YR in IL–ATPS where the ionic liquid used is [Bmim]BF<sub>4</sub> and salts include (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub> and MnSO<sub>4</sub>. Unlike the previously mentioned polymer based ATPS, YR partitions preferentially to the bottom phase in the IL–ATPS.

To understand the variation of  $K_{\rm YR}$  values with respect to TLL, it is necessary evaluate both the entropic and enthalpic contributions. As the TLL increases, so does the concentration of the components in each phase and therefore there is a greater number of interactions between YR and the main interacting component.



**Fig. 5.** Effect of cation of the salt forming ATPS on the YR partition behavior: ( $\blacktriangleright$ ) [Bmim]BF<sub>4</sub>+MnSO<sub>4</sub>+H<sub>2</sub>O, ( $\triangleright$ ) [Bmim]BF<sub>4</sub>+(NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>+H<sub>2</sub>O.

This will therefore modify the first term of Eq. (6), by increasing the enthalpic contribution of the  $K_{YR}$  value.

On the other hand, the difference in the amount of water between the bottom and top phase is altered (Table 4); consequently, the term  $((n^T/V^T) - (n^B/V^B))$  in Eq. (7) becomes more negative or more positive, changing entropic contribution for transfer of YR between phases of the ATPS.

In  $[Bmim]BF_4 + (NH_4)_2SO_4 +$  water ATPS, the top phase is rich in IL, the bottom phase rich in salt and water is the predominant component in both phases. The YR partition behavior in this system is attributed to an entropic contribution resulting in an increase in the dye partition coefficient with increasing TLL.

However in [Bmim]BF<sub>4</sub>+MnSO<sub>4</sub>+water  $K_{YR}$  decreases with increasing TLL. This surprising partitioning behavior can be rationalized by considering that this system exhibits phase inversion. Therefore, the IL-enriched phase which is the less dense top phase, becomes the bottom phase for TLL 3–5 [21].

At smaller TLL values, partitioning of YR is enthalpically driven and for this reason, this dye tends to migrate preferential to the bottom phase due to interactions with the IL. Interestingly, when the TLL increases, the number density of the salt-rich phase is higher than that of IL-rich phase (Table 4) due to the major water content in the bottom phase. Thus, the entropic contribution predominates with regard to the enthalpic contribution, resulting in a decrease in  $K_{YR}$  values.

Previous studies by Ferreira et al. [4] demonstrated that textile dyes chloranilic acid, indigo blue and sudan III migrate to the superior phase of the IL-ATPS formed from a combination of different IL and electrolytes. Ventura et al. [36] also observed partition coefficient values greater than unity for natural red colorants isolated from fermented broth. These results show the enormous potential of IL for the removal of dyes from industrial effluents.

# 3.7. Extraction efficiency of YR in ATPS

The extraction efficiency ( $\%E_{YR}$ ) of YR is an important parameter used to evaluate the capacity of ATPS to extract this dye from aqueous matrices to the upper phase of the ATPS. For all of the ATPS composed of polymer and salt, the  $\%E_{YR}$  obtained was equal to superior than 97% and highlighting furthermore the potential of this method. The only exception was the TLL 1 to the system PEG 1500+sodium tartrate+water, which was 87%. The  $\%E_{YR}$  in the system formed from PEG 1500+LiSO<sub>4</sub>+H<sub>2</sub>O as a function of the TLL is shown in Fig. 6.

For this system, the  $\%E_{YR}$  values are superior than 99% and show clearly the high capacity of the ATPS to remove and extract YR.

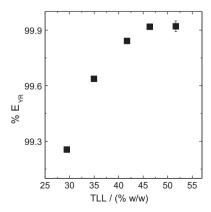


Fig. 6. Extraction efficiency of YR in ATPS PEG 1500 + Li<sub>2</sub>SO<sub>4</sub> + H<sub>2</sub>O.

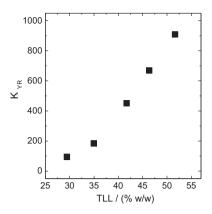


Fig. 7. Partition behavior of YR in presence of wastewater.

Table 5 Recovery values of the YR for PEG 1500 + Li<sub>2</sub>SO<sub>4</sub> + H<sub>2</sub>O ATPS at 298 K.

TLL (%m/m)	Top phase recovery (%		
29.43	$100.5 \pm 0.5$		
34.97	$103.2\pm0.9$		
41.71	$94.7 \pm 0.7$		
46.36	$99.7 \pm 0.3$		
51.67	$98.2 \pm 0.7$		

Notably, at the first TLL, the  $\%E_{YR}$  is 99.2. This is a very positive result when we consider future applications on a large industrial scale given how at the first TLL, the concentration of the components that form the ATPS are lower and so improve the cost benefit of the process for treating effluents.

On the other hand, in the case of IL-ATPS when the TLL increased, the  $%E_{YR}$  also increased from 7.07 to 9.12 in [Bmim]  $BF_4 + (NH_4)_2SO_4 +$  water and decreased from 15.8 to 8.65 in [Bmim] BF<sub>4</sub> + MnSO<sub>4</sub> + water, demonstrating the potential removal of YR in aqueous matrices to the lower phase of the IL-ATPS.

# 3.8. Recovery of YR in presence of waste water

To determine the concentration of YR in the presence of textile effluent without matrix effects, the standard addition method was performed. The waste water stock solution was used as solvent to prepare the ATPS. The partition coefficients revealed the dye partitions toward the top phase of the ATPS, as shown in Fig. 7.

Table 5 shows the results for our recovery studies in wastewater samples. The results indicate that in the case of the effluent sample, in spite of the presence of other components (i.e. metals, surfactants and other dyes) this ATPS is able to remove the dye with extraction efficiency close to 100% for all TLL evaluated.

# 4. Conclusion

This work demonstrates the possible use of ATPS as a methodology for the removal of the synthetic dye YR from wastewater. Several parameters were evaluated in order to understand the partitioning of YR in ATPS. Thermodynamic parameters such as  $\Delta_{\rm tr}G^{\circ}$  were determined and used in conjunction with the Johansson model to explain partitioning behaviors. This model reveals that the higher concentration of YR in the top phase in polymer-ATPS systems is enthalpically directed. In contrast, the dye moves to the bottom phase of ATPS that contain IL. Interestingly, the driving force that governs this process depends on the salt that is utilized in this mixture and the difference between the intensive thermodynamic properties of ATPS phases (TLL).

Maximum values for  $K_{YR}$  were observed for ATPS formed by PEG 1500 + Li<sub>2</sub>SO<sub>4</sub> + H<sub>2</sub>O and for this system, a strong Li<sup>+</sup> cation effect was noted. The molecular mass of the polymer and the nature of the anion showed no significant effect on the YR partitioning behavior. This system was applied with success to the removal of YR from wastewater. The high  $K_{YR}$  values in the presence of the effluent demonstrate the potential of the ATPS in the treatment of effluents from textile industries...

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